# Appendix A:

Transportation Conditions Analysis Memorandum



To: Ms. Lara Justesen

From: Shashi Gannavaram, P.E, PTP, AICP, PTOE

CC:

Date: 9/24/2013

Re: Transportation conditions analysis for the Englewood Arts District

#### 1 Introduction

R^3C Design Group, LLC was requested to assist in transportation planning and traffic engineering elements for developing a Circulation Plan for the Englewood Arts District in Independence, Missouri. The Englewood Arts District is on E. Winner Road between Northern Boulevard and Sterling Road.

In particular the existing roadway system in the district is evaluated, including crash rates, the unique median parking and sight-distance challenges. Because the intersection of E. Winner Road and Northern Boulevard, on the west edge of the district, is a complicated five-legged

intersection, much of this document describes the inherent challenges of this area and offers positive alternatives for improving the intersection. Finally, priorities are presented for improving the overall traffic flow through the district - both auto and non-motorized.

The arts district is predominantly commercial, including only a few residences on the western end of the project, near Northern Boulevard. The commercial district is



**Exhibit 1: Looking west along E. Winner Road** 

comprised mostly of small, personally-owned and operated businesses, providing a wide range of services. The corridor's key attraction is the now-closed Englewood Theater, which has no immediate plan to reopen.

The sidewalks and northern curb line between Sterling Road and Appleton Avenue have been recently improved by the City of Independence. This project also included new crosswalks and



pedestrian signs at key intersections. There are no immediate Capital Improvement Projects planned on E. Winner Road.

### 2 Roadway system

### 2.1 Crash analysis

Crash data from 2010 to July 2013 was obtained from the City of Independence and analyzed to detect any unsafe conditions. The crash data was on E. Winner Road between Northern Avenue and Sterling Avenue. The data is summarized in Exhibit 3 below.

The following observations were noted:

- 36-percent (4 of 11) of the crashes resulted in injuries.
- There were no pedestrian vehicle crashes in the corridor.
- Failing to yield resulted in 45% (5 of 11) crashes.
- In the last three years, the Northern Avenue intersection has seen no crashes. The closest crash occurred 50 feet east of Northern Avenue as a car was merging into traffic.
- The Appleton Avenue intersection experienced 45% (5 of 11) crashes in the corridor.
  - Police reports indicated that two of the crashes resulted from obscured vision due to a parked car on the west side of the intersection.

Further review of the Appleton Avenue intersection reveals the following:

 Sight distance restrictions – Sight distance restrictions are primarily due



Looking east at Appleton Avenue



Exhibit 2: Sight distance challenges due to parked vehicles at Appleton Avenue





to the angled parking along on-street medians. Since sight triangles are not strictly observed at this location, cars in the median are not able to view traffic on E. Winner Road during the turn. An example of these restrictions is shown in Exhibit 2.

Year	Location	Severity	Number of vehicles	Туре	Cause	Notes	Harvard St.
	50 feet east of Northern	PDO	2	Sideswipe	Failure to yield		
	Winner Road - mid- block	INJ	2	Head on	Too fast		
2010	Appleton at Winner	PDO	2	Right angle	Failure to yield	Vision obscured by parked car on west side	
	Appleton at Winner	INJ	2	Right angle	Failure to yield	Vision obscured by parked car on west side	S. Harris Ave.
	45 feet east of Harris	PDO	2	Parked car	Improper backing	Bad pull out from parking stall	
	Appleton at Winner	PDO	2	Angle	Improper signal + inattention		ner Road
20	Appleton at Winner	PDO	2	Sideswipe	Improper passing		E. Win
	Harvard at Winner	INJ	2	Angle	Failure to yield		S. Appleton Ave.
7	Winner Road at alley near Englewood Café	PDO	1	Drive into construction zone	Inattention		
	Appleton at Winner	INJ	2	Angle	Failure to yield		
$\dot{c}$	50 feet west of Harvard	PDO	2	Parked car	Poor lane use		1
2. INJ	s: O = Property damago = Injury crash ash reports between			l July 22, 2013	summarized		S. Northern Blvd.  Crash location and number

**Exhibit 3: Crash analysis on E. Winner Road** 

### 2.2 On-street median parking

A very unique feature of the Englewood Arts District, specifically E. Winner Road, is the onstreet angled median parking. Business owners on E. Winner Road consider this long-standing feature sacred and strongly oppose any change to this parking pattern. However, significant challenges are posed by the on-street median parking.



Adjoining lane width:
 The 60-degree angled parking results in a very wide lane width for vehicular traffic.
 In some locations, each lane on E.
 Winner Road is about 22 feet wide. Even though this section of the



**Exhibit 4: On-street median parking** 

- roadway is posted at 20 miles per hour (mph), the excessive pavement increases the comfort of the driver, and higher speeds tend to prevail.
- <u>Sight distance:</u> The median parking restricts the sight triangle particularly for vehicles turning onto the side streets. This is one of the primary factors for the higher crash rate at the Appleton Avenue intersection. The crash rates are discussed in a prior section.
- <u>Crossing E. Winner Road:</u> Business patrons park in the median and conveniently cross the street in front of their car at mid-block locations. Oncoming drivers must be unduly cautious of pedestrians stepping out from behind a parked car in the median.

Because of the wide lane width, a suggestion was presented to the steering committee to reduce the angle of the parking from the current 60 degrees to 45 degrees. This angle reduction also reduces the required lane width to 12 feet, with a stall width of 8 feet, a depth of 18.5 feet and skew width of 11.3 feet. However, it should be noted that the current city standard for parking stall width is 9 feet.

By reducing the parking angle and lane widths pedestrian safety is improved because of the shorter walking distance and exposure time in mid-block locations. Significantly, the spatial restrictions perceived by drivers will assist in slowing the vehicular traffic.

While this solution does not address the concerns listed above, it does maintain the desired onstreet parking while providing some safety enhancements.

### 2.3 Sight distance

A significant cause for concern and safety is the sight distance challenges posed by large vehicles parking in the median near side street intersections. The plane of the sight triangle is encroached upon, causing vision challenges for traffic crossing E. Winner Road. This vision challenge must be recognized by those implementing future roadway improvements, and appropriate guidelines must be followed. These are provided in the "A Policy on Geometric Design of Highways and Street," published by the American Association of State Highway and



Transportation Officials (AASHTO), 2004 (commonly referred to as the green book). The criteria are as follows:

- Left turn from stop (Exhibit 9-55 of the green book)
  - o 280-feet for 25 mph
  - o 225 feet for 20 mph
- Crossing maneuver (Exhibit 9-58 of the green book)
  - o 240-feet for 25 mph
  - o 195 feet for 20 mph

During concept plan development, the guidelines were used to determine the triangle at each crossing point. Because business owners were unwilling to give up three or four parking spots at each crossing, an alternative plan was developed to minimize the sight triangle encroachment. This plan utilized green space and parking spaces specifically designated to compact cars and bicycles. . Exhibit 5 shows the final concept developed for the Appleton Avenue intersection.

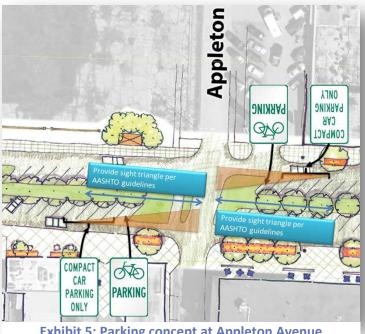


Exhibit 5: Parking concept at Appleton Avenue intersection

#### 3 E. Winner Road at Northern Avenue Intersection

E. Winner Road at Northern Avenue, located on the west edge of the study area, is a non-standard five-legged intersection. An in-depth analysis is being completed for this intersection to determine possible improvements and create a gateway entrance to the arts district.



### 3.1 Existing traffic counts

Traffic counts were collected in July 2013 during the morning and afternoon peak hours. Pedestrian activity was also recorded during the same time periods. These counts are shown in Exhibit 6 below.



Exhibit 6: Existing traffic counts at E. Winner Road and Northern Boulevard intersection



Exhibit 7: No pedestrian actuation at E. Winner Road and Northern Boulevard

From these traffic counts we observe the following:

• Pedestrian activity is minimal during both peak auto-traffic periods. While the intersection is a non-standard five-legged intersection, it is believed to be relatively simple to access and cross. Although the existing signal has pedestrian indications, no push-buttons are provided for pedestrian actuation.



- Traffic flow is not directional the volume of traffic east or westbound on E. Winner Road is of the same magnitude during both peak periods.
- Minimal traffic is turning onto E. 18<sup>th</sup> Street. Most of the E. 18<sup>th</sup> Street traffic continues as through traffic from the east leg of E. Winner Road.
- During field observations, it was noted that the majority of the traffic to E. 18<sup>th</sup> Street is turning one block west at S. Ralston Avenue.

### 3.2 Capacity analysis

When evaluating modifications to an intersection its operational level must be established. Based upon the delays experienced by its users, a baseline is set and improvement ideas are analyzed. Any alternatives developed should exceed this baseline level of operations. The "Highway Capacity Manual", published by the Transportation Research Board (TRB), 2010 provides guidelines for completing an operational analysis at the intersection. The analysis

results in a letter grade called the Level of Service (LOS). LOS ranges from A through F where LOS A implies drivers experience no delays while LOS F indicates a complete breakdown at the intersection. For signalized intersections, the criteria for the LOS grade are shown in the adjacent table.

Level of Service (LOS)	Delay (seconds per vehicle)	General description
Α	≤ 10	Free flow
В	>10 to 20	Stable flow
С	>20 to 35	Stable flow
D	>35 to 55	Tolerable delay
E	>55 to 80	Intolerable delay
F	>80	Jammed conditions

**Exhibit 8: Signal intersection level of service criteria** 

Because this intersection is five-

legged, it should be noted that the HCM 2010 methodology does not analyze it. HCM 2000 methodologies were used to complete the analysis. The criteria used for determining the LOS is the same using both methodologies. However, minor modifications do exist in how the delay is calculated.

The analysis is completed using software called <u>Synchro</u>, released by Trafficware, version 8. The results of the analysis are shown in Exhibit 9. Outputs from the software are included in the appendix. The following conclusions are made from the analysis results.



	Peak				Approach			Intersection
ts	hour/ item		18 <sup>th</sup> St. Eastbound	Winner Rd. Westbound	Northern Northbound	Northern Southbound	Winner Eastbound	
lysis resul		Delay*	15.6	11.8	4.4	4.4	16.8	12.1
acity Ana	Morning	SOI	В	В	А	А	В	В
Existing Capacity Analysis results	no	Delay*	11.9	9.4	6.9	7.1	15.4	11.4
ă	Afternoon	SOI	В	А	А	А	В	В

<sup>\* -</sup> delay is measured in seconds per vehicle

**Exhibit 9: Existing capacity analysis summary** 

From Exhibit 9 it is observed that the intersection can meet its present traffic demand. The levels-of-service are indicative of minimal delays. Further, it is believed that sufficient spare capacity is available to accommodate future growth.

### 3.3 Alternative development

This phase was primarily completed during the charrette on August 5 and 6, 2013. The steering committee and the Transportation Focus Group were presented with the existing conditions. During the discussions, it was noted that the E. 18<sup>th</sup> Street leg of the intersection was primarily funneling traffic to and from E. Winner Road. Good connectivity within the network allows traffic to turn onto E. 18<sup>th</sup> Street from S. Ralston Avenue to the west and E. 19<sup>th</sup> Street to the south.

Simplifying the intersection was a primary desire of the steering committee and a suggestion was made to close E. 18<sup>th</sup> Street at S. Hedges Avenue. This would force S. Hedges Avenue traffic to use E. 18<sup>th</sup> Street to the west, using S. Ralston Avenue to connect to E. Winner Road.

The advantages of this approach are:

- 1. The five legged intersection of S. Northern Boulevard and E. Winner Road becomes a standard four legged intersection.
- 2. Traffic coming to and from S. Hedges Avenue has a standard four-way intersection at S. Ralston Avenue.



However, a disadvantage is that S. Hedges Avenue traffic must travel an extra distance to get to E. Winner Road. Traffic heading east on E. Winner Road will be the most inconvenienced with this approach.

The overall approach of closing E. 18<sup>th</sup> Street between S. Hedges Avenue and E. Winner Road was very well received by the steering committee. This modified intersection is shown in Exhibit 10.



**Exhibit 10: Proposed four-legged intersection** 

Because the intersection is now converted to a standard four-way intersection, options for traffic control are discussed. A desire of the focus group is to convert this intersection into a gateway to the Englewood Arts District. The two options that present themselves are:

- 1. Improve the signal layout at the intersection or
- 2. Install a single-lane roundabout at the intersection.

These are shown in Exhibit 11. Because of the overwhelming support for standardizing the intersection by closing the E. 18<sup>th</sup> Street leg, further analysis and alternative testing is being completed using each of these two alternatives.



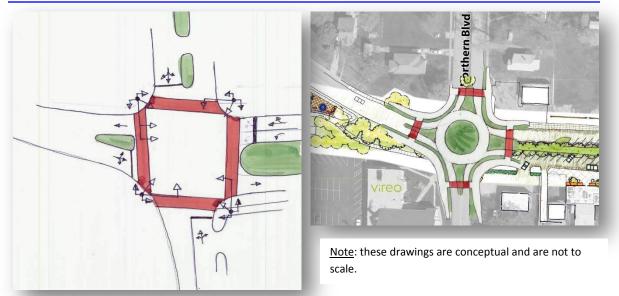


Exhibit 11: Alternatives for the E. Winner Road and Northern Boulevard intersection

Advantages and disadvantages for each method of traffic control were briefly presented during the charrette. A few of these are summarized in Exhibit 12. Despite the disadvantages of a roundabout, the steering group and the charrette attendees unanimously prefer a roundabout for this intersection.

Signal int	ersection	Round	labout
Advantages	Disadvantages	Advantages	Disadvantages
	32 points of conflict between vehicles and pedestrians	Safer  Reduced vehicle speed Reduction in conflict points	
Shorter walking distance for the pedestrian	Increased exposure for pedestrians	Reduced exposure for pedestrians	Increased walking distance for a pedestrian
	Increased congestion	Reduced congestion	
	Maintenance for life of signal	Reduced maintenance costs – primarily landscaping	
	Increased fuel use and pollution	Reduced fuel use and pollution	
Users are used to signals – no learning required.			Not used to a roundabout – learning curve required

Exhibit 12: Advantages and disadvantages of intersection control



### 3.4 Alternative testing

Alternative testing uses current counts to determine operational performance levels. These are compared to the existing levels-of-service, from Exhibit 9, and a suitable approach for traffic control at the intersection is selected. The two tested alternatives are:

- 1. Standard four-way intersection with a signal
- 2. Standard four-way intersection with a single lane roundabout.

Results of this analysis are summarized in Exhibit 13. For both scenarios, the results indicate the intersection will operate at a high level of service. The intersection is projected to operate at LOS B with a signal control and LOS A with a roundabout.

To ensure that the intersection option will fulfill demand needs for the design life of 20 years, the two scenarios are tested by increasing existing traffic volumes at a two-percent (2%) annual growth rate. This increases the traffic by about 50% over the 20-years. These results are summarized in Exhibit 14. In 20 years the intersection is projected to continue operating at LOS B with signal control and LOS A with a roundabout in place.

Roundabout parameters used for analysis are as follows:

- Because the available diagonal pavement at the intersection is approximately 95 feet, the outside diameter of the roundabout was set at 90-feet.
- The circulatory lane width is set at 15 feet.
- The inside circle diameter is 60 feet.
- All approach radii are set at a 50 feet radius.
- Lane width for approaching and exiting lanes is set at 12 feet, due to Kansas City Area Transportation Authority (KCATA) busses that use E. Winner Road.
- Pedestrian crosswalks are set 25 feet behind the yield line for each approach.
- Roundabout analysis was completed using the software SIDRA, released by Ackelick and Associates, version 6.



ম	Peak	(		Appr	oach		Intersection
s resul	hour item		Winner Rd. Westbound	Northern Northbound	Northern Southbound	Winner Rd. Eastbound	<b>.</b>
ty Analysi :tion :ounts		Delay*	13.4	4.2	4.3	15.2	12.3
emoved Capacity Ana Signal intersection Existing traffic counts	Morning	SOI	В	А	А	В	В
18 <sup>th</sup> Street removed Capacity Analysis results Signal intersection Existing traffic counts	E.	Delay*	12.7	7.4	7.4	14.8	12.7
18 <sup>th</sup> Stre	Afternoon	SOT	В	А	А	В	В
ts	Peak			Intersection			
s resu	hour item		Winner Rd. Westbound	Northern Northbound	Northern Southbound	Winner Rd. Eastbound	10=
18 <sup>th</sup> Street removed Capacity Analysis results Roundabout intersection Existing traffic counts	bo	Delay*	4.5	4.0	4.0	4.5	4.4
: removed Capacity Analy Roundabout intersection Existing traffic counts	d Capacit		А	А	А	А	А
et remov Rounda Existir	L.	Delay*	5.7	5.4	4.8	6.9	6.1
18 <sup>th</sup> Stre	Afternoon	SOT	А	А	А	А	А

Exhibit 13: Proposed four-legged intersection capacity analysis summary



S.	Peak			Appr	oach		Intersection
s result	hour item		Winner Rd. Westbound	Northern Northbound	Northern Southbound	Winner Rd. Eastbound	8
ty Analysi :tion olumes		Delay*	13.0	5.1	5.2	15.3	12.4
removed Capacity Anal Signal intersection 20-year traffic volumes	Morning	SOI	В	А	А	В	В
18 <sup>th</sup> Street removed Capacity Analysis results Signal intersection 20-year traffic volumes	u	Delay*	13.4	10.1	10.1	17.0	14.4
18 <sup>th</sup> Stre	Afternoon	SOI	В	В	В	В	В
ts	Peak			Intersection			
s resu	hour item		Winner Rd. Westbound	Northern Northbound	Northern Southbound	Winner Rd. Eastbound	No.
ty Analysis resu rsection olumes	item						4.9
ed Capacity Analysis resu Ibout intersection r traffic volumes			Westbound	Northbound	Southbound	Eastbound	4.9 A
18 <sup>th</sup> Street removed Capacity Analysis results Roundabout intersection 20-year traffic volumes	item	Delay*	Westbound 5.1	Northbound 4.4	Southbound 4.4	Eastbound 5.1	

Exhibit 14: 20-year capacity analysis summary

### 4 Priorities

The existing transportation conditions analysis for the Englewood Arts District was completed by the R^3C Design Group, LLC. The focus was on the existing roadway conditions, crash rates, median parking and the sight distance restrictions caused by the on-street parking. However, the primary charge was to develop alternatives for the five-legged intersection at E. Winner Road and Northern Boulevard.



### 4.1 Roadway system

Field observations and the analysis indicate an excessive amount of pavement for accommodating one lane of traffic in each direction. At some locations the pavement was as wide as 22 feet, where a 12-feet lane width is adequate for traffic movement.

A cause of this wide pavement is the angled median parking. Because the entry angle is 60-degrees, wider pavement width is required to negotiate the parking spot. By reducing this parking angle to 45-degrees, a narrower lane width is used by the through vehicles. An added benefit is the shorter distance and time that it takes for the pedestrians to cross E. Winner Road.

As part of this section, the crash rates and the predominant causes of crashes on E. Winner Road are examined. The high crash location is at Appleton Avenue and the main cause of the crashes is a lack of sight distance for traffic turning onto Appleton Avenue from E. Winner Road. When cars are parked in the median parking spots, the sight triangle is penetrated and turning vehicles are unable to see approaching traffic.

#### 4.2 E. Winner Road and Northern Boulevard intersection

The data reveals that the traffic proceeds through this intersection because of the complicated nature of making a turn. The preferred turning location is S. Ralston Street, one block to the west. After considering the data and input from the steering committee and charrette participants, the E. 18<sup>th</sup> Street connection between S. Hodges Road and E. Winner Road is eliminated.

This change improves the intersection to a standard four-way intersection, while causing only a minor inconvenience to the traffic on S. Hodges Avenue, as they are routed along S. Ralston Avenue to get to E. Winner Road.

Using the four-legged intersection as a basis, two alternatives for traffic control are evaluated and discussed in the charrette. A capacity analysis for both alternatives reveals that the intersection would operate with no delays regardless of the intersection control. However, charrette participants overwhelmingly approved the roundabout concept because of the inherent safety features.



## 5 Appendix



## 5.1 Existing

## 5.1.1 Morning peak hour

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			14.6	Tartinens co		320				122	. 7	100000000
Movement	EBT	EBR	WBL	WBT	WBR	WBR2	NBL	NBT	NBR	SBL	SBT	SEL
Lane Configurations	4		ሻ	<b>^</b>	7		- 0	4			4	
Volume (vph)	26	1	9	10	92	25	5	10	13	20	11	
ldeal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)	4.0		4.0	4.0	4.0			4.0			4.0	
Lane Util. Factor	1.00		1.00	1.00	1.00			1.00			1.00	
Frt	1.00		1.00	1.00	0.85			0.94			1.00	
Fit Protected	1.00		0.95	1.00	1.00			0.99			0.97	
Satd. Flow (prot)	1854		1770	1863	1583			1731			1804	
Fit Permitted	1.00		0.74	1.00	1.00			0.98			0.90	
Satd. Flow (perm)	1854		1375	1863	1583			1710			1672	
Peak-hour factor, PHF	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	28	1	10	11	100	27	5	11	14	22	12	
RTOR Reduction (vph)	1	0	0	0	81	0	0	6	0	0	0	(
Lane Group Flow (vph)	28	0	10	11	46	0	0	24	0	0	34	(
Tum Type	NA		pm+pt	NA	Perm		Perm	NA		Perm	NA	Perm
Protected Phases	4!		3	8!				2			6	
Permitted Phases			8		8		2			6		4
Actuated Green, G (s)	6.2		10.9	10.9	10.9			22.9			22.9	
Effective Green, g (s)	6.2		10.9	10.9	10.9			22.9			22.9	
Actuated g/C Ratio	0.15		0.26	0.26	0.26			0.55			0.55	
Clearance Time (s)	4.0		4.0	4.0	4.0			4.0			4.0	
Vehicle Extension (s)	3.0		3.0	3.0	3.0			3.0			3.0	
Lane Grp Cap (vph)	274		365	485	412			936			916	
v/s Ratio Prot	0.02		0.00	0.01								
v/s Ratio Perm			0.01		c0.03			0.01			c0.02	
w/c Ratio	0.10		0.03	0.02	0.11			0.03			0.04	
Uniform Delay, d1	15.4		11.5	11.5	11.8			4.3			4.4	
Progression Factor	1.00		1.00	1.00	1.00			1.00			1.00	
Incremental Delay, d2	0.2		0.0	0.0	0.1			0.0			0.1	
Delay (s)	15.6		11.5	11.5	11.9			4.4			4.4	
Level of Service	В		В	В	В			Α			А	
Approach Delay (s)	15.6			11.8				4.4			4.4	
Approach LOS	В			В				Α			Α	
Intersection Summary												
HCM 2000 Control Delay			12.1	Н	ICM 2000	Level of :	Service		В			
HCM 2000 Volume to Capac	ity ratio		0.11									
Actuated Cycle Length (s)			41.8	S	um of los	t time (s)			12.0			
Intersection Capacity Utilizati	ion		26.8%	10	CU Level	of Service			Α			
Analysis Period (min)			15									

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4:				- 8/
VV	<b>\</b>	>	4	
Movement	SEL	SER	SER2	
Lane Configurations	M		7	
Volume (vph)	79	7	Ö	
Ideal Flow (vphpl)	1900	1900	1900	
Total Lost time (s)	4.0			
Lane Util. Factor	1.00			
Frt	0.99			
Fit Protected	0.96			
Satd. Flow (prot)	1759			
Fit Permitted	1.00			
Satd. Flow (perm)	1832			
Peak-hour factor, PHF	0.92	0.92	0.92	
Adj. Flow (vph)	86	8	0	
RTOR Reduction (vph)	0	0	0	
Lane Group Flow (vph)	95	0	0	
Tum Type	NA	***	Perm	
Protected Phases	4!			
Permitted Phases			4	
Actuated Green, G (s)	6.2			
Effective Green, g (s)	6.2			
Actuated g/C Ratio	0.15			
Clearance Time (s)	4.0			
Vehicle Extension (s)	3.0			
Lane Grp Cap (vph)	271			
v/s Ratio Prot	77.00			
v/s Ratio Perm	c0.05			
v/c Ratio	0.35			
Uniform Delay, d1	16.0			
Progression Factor	1.00			
Incremental Delay, d2	0.8			
Delay (s)	16.8			
Level of Service	В			
Approach Delay (s)	16.8			
Approach LOS	В			

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## 5.1.2 Afternoon peak hour

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Movement	EBT	WBL	WBT	WBR	WBR2	NBL	NBT	NBR	SBL	SBT	SBR	SBR
Lane Configurations	4	7	1	7			4		24000	4		
Volume (vph)	26	19	26	159	34	10	20	28	38	20	1	2
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)	4.0	4.0	4.0	4.0			4.0			4.0		
Lane Util. Factor	1.00	1.00	1.00	1.00			1.00			1.00		
Frt	1.00	1.00	1.00	0.85			0.94			0.99		
Fit Protected	1.00	0.95	1.00	1.00			0.99			0.97		
Satd. Flow (prot)	1863	1770	1863	1583			1728			1796		
Flt Permitted	1.00	0.74	1.00	1.00			0.97			0.86		
Satd. Flow (perm)	1863	1377	1863	1583			1686			1586		
Peak-hour factor, PHF	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	28	21	28	173	37	11	22	30	41	22	1	2
RTOR Reduction (vph)	0	0	0	69	0	0	17	0	0	1	0	(
Lane Group Flow (vph)	28	21	28	141	0	0	46	0	0	65	0	(
Tum Type	NA	pm+pt	NA	Perm		Perm	NA		Perm	NA		-
Protected Phases	41	3	8!				2			6		
Permitted Phases		8		8		2			6			
Actuated Green, G (s)	10.9	15.5	15.5	15.5			18.8			18.8		
Effective Green, g (s)	10.9	15.5	15.5	15.5			18.8			18.8		
Actuated g/C Ratio	0.26	0.37	0.37	0.37			0.44			0.44		
Clearance Time (s)	4.0	4.0	4.0	4.0			4.0			4.0		
Vehicle Extension (s)	3.0	3.0	3.0	3.0			3.0			3.0		
Lane Grp Cap (vph)	480	510	682	580			749			704		
w/s Ratio Prot	0.02	0.00	0.02									
v/s Ratio Perm		0.01		c0.09			0.03			c0.04		
v/c Ratio	0.06	0.04	0.04	0.24			0.06			0.09		
Uniform Delay, d1	11.8	8.6	8.6	9.3			6.7			6.8		
Progression Factor	1.00	1.00	1.00	1.00			1.00			1.00		
Incremental Delay, d2	0.1	0.0	0.0	0.2			0.2			0.3		
Delay (s)	11.9	8.7	8,6	9.5			6.9			7.1		
Level of Service	В	Α	Α	Α			Α			Α		
Approach Delay (s)	11.9		9.4				6.9			7.1		
Approach LOS	В		Α				Α			Α		
Intersection Summary												
HCM 2000 Control Delay 11.4				E	ICM 2000	Level of :	Bervice		В			
HCM 2000 Volume to Capacity ratio 0.29												
Actuated Cycle Length (s) 42.3			Sum of lost time (s)					12.0				
Intersection Capacity Utilization 41.0%			P	CU Level (	of Service			Α				

Baseline Synchro \$ Report Page 1





	•	<b>\</b>	7	4
Movement	SEL2	SEL	SER	SER2
Lane Configurations		M		7
Volume (vph)	2	228	19	0
Ideal Flow (vphpl)	1900	1900	1900	1900
Total Lost time (s)		4.0		
Lane Util, Factor		1.00		
Frt		0.99		
Fit Protected		0.96		
Satd. Flow (prot)		1760		
Fit Permitted		1.00		
Satd. Flow (perm.)		1837		
Peak-hour factor, PHF	0.92	0.92	0.92	0.92
Adj. Flow (vph)	2	248	21	0
RTOR Reduction (vph)	0	0	0	0
Lane Group Flow (vph)	0	271	0	0
Tum Type	Perm	NA		Perm
Protected Phases		4!		
Permitted Phases	4!			4
Actuated Green, G (s)		10.9		
Effective Green, g (s)		10.9		
Actuated g/C Ratio		0.26		
Clearance Time (s)		4.0		
Vehicle Extension (s)		3.0		
Lane Grp Cap (vph)		473		
w/s Ratio Prot				
v/s Ratio Perm		c0.15		
w/c Ratio		0.57		
Uniform Delay, d1		13.7		
Progression Factor		1.00		
Incremental Delay, d2		1.7		
Delay (s)		15.4		
Level of Service		В		
Approach Delay (s)		15.4		
Approach LOS		В		

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## 5.2 18th Street removed with current year traffic counts

### 5.2.1 Signal control

### 5.2.1.1 Morning peak hour

HCM 2010 Signalized Intersection Summary
4: \$12502013

	۶	-	7	1	•	•	1	1	1	1	Į.	1
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBF
Lane Configurations		4	47947	7	1	2000		4	1775	100000	4	
Volume (veh/h)	1	105	7	19	92	25	5	10	13	20	11	0
Number	7	4	14	3	8	18	5	2	12	1	6	16
Initial Q (Qb), veh	0	0	0	0	0	0	0	0	0	0	0	C
Ped-Bike Adj(A_pb T)	1.00		1.00	1.00		1.00	1.00		1.00	1.00		1.00
Parking Bus Adj	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Adj Sat Flow veh/h/ln	190.0	186.3	190.0	186.3	186.3	190.0	190.0	186.3	190.0	190.0	186.3	190.0
Lanes	0	1	0	1	1	0	0	1	0	0	1	0
Cap, veh/h	105	206	14	37	362	98	198	382	403	645	318	0
Arrive On Green	0.12	0.12	0.12	0.02	0.26	0.26	0.52	0.52	0.52	0.52	0.52	0.00
Sat Flow, veh/h	8	1711	120	1774	1414	382	151	742	781	923	617	0
Grp Volume(v), veh/h	123	0	0	21	0	127	30	0	.0	34	0	0
Grp Sat Flow(s), veh/h/ln	1838	0	0	1774	0	1795	1675	0	0	1540	0	0
Q Serve (q s), s	0.2	0.0	0.0	0.4	0.0	2.0	0.0	0.0	0.0	0.0	0.0	0.0
Cycle Q Clear(q_c), s	2.2	0.0	0.0	0.4	0.0	2.0	0.3	0.0	0.0	0.3	0.0	0.0
Prop In Lane	0.01		0.07	1.00		0.21	0.17		0.47	0.65		0.00
Lane Grp Cap(c), veh/h	325	0	0	37	0	460	983	0	0	963	0	0
V/C Ratio(X)	0.38	0.00	0.00	0.56	0.00	0.28	0.03	0.00	0.00	0.04	0.00	0.00
Avail Cap(c a), veh/h	944	0	0	203	0	1233	983	0	0	963	0	C
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Upstream Filter(I)	1.00	0.00	0.00	1.00	0.00	1.00	1.00	0.00	0.00	1.00	0.00	0.00
Uniform Delay (d), s/veh	14.5	0.0	0.0	16.9	0.0	10.4	4.2	0.0	0.0	4.2	0.0	0.0
Incr Delay (d2), s/veh	0.7	0.0	0.0	12.5	0.0	0.3	0.1	0.0	0.0	0.1	0.0	0.0
Initial Q Delay(d3),s/veh	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
%ile Back of Q (50%), veh/ln	0.9	0.0	0.0	0.3	0.0	0.7	0.1	0.0	0.0	0.1	0.0	0.0
Lane Grp Delay (d), s/veh	15.2	0.0	0.0	29.4	0.0	10.7	4.2	0.0	0.0	4.3	0.0	0.0
Lane Grp LOS	В			С		В	Α			Α		
Approach Vol., veh/h		123			148			30		1,000	34	
Approach Delay, s/veh		15.2			13.4			4.2			4.3	
Approach LOS		В			В			Α			A	
Timer					,,,							
Assigned Phs		4		3	8			2			6	
Phs Duration (G+Y+Rc), s		8.2		4.7	12.9			22.0			22.0	
Change Period (Y+Rc), s		4.0		4.0	4.0			4.0			4.0	
Max Green Setting (Gmax), s		16.0		4.0	24.0			18.0			18.0	
Max Q Clear Time (q_c+l1), s		4.2		2.4	4.0			2.3			2.3	
Green Ext Time (p_c), s		0.4		0.1	0.7			0.2			0.2	
Intersection Summary												
HCM 2010 Ctrl Delay			12.3									
HCM 2010 LOS			В									
Notes												

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### 5.2.1.2 Afternoon peak hour

HCM 2010 Signalized Intersection Summary

8/24/201	

	•	-	7	1	•	•	4	1	1	1	Į.	1
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBF
Lane Configurations		43		*	<b>^</b>	71-971	0.7100	4			ન	
Volume (veh/h)	3	264	20	45	159	34	10	20	28	38	20	3
Number	7	4	14	3	8	18	5	2	12	1	6	16
Initial Q (Qb), veh	0	0	0	0	0	0	0	0	0	0	0	0
Ped-Bike Adj(A_pbT)	1.00		1.00	1.00		1.00	1.00		1.00	1.00		1.00
Parking Bus Adj	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Adj Sat Flow veh/h/ln	190.0	186.3	190.0	186.3	186.3	190.0	190.0	186.3	190.0	190.0	186.3	190.0
Lanes	0	1	0	1	1	0	0	1	0	0	1	Ò
Cap. veh/h	90	423	32	74	578	124	169	298	330	501	245	29
Arrive On Green	0.25	0.25	0.25	0.04	0.39	0.39	0.42	0.42	0.42	0.42	0.42	0.42
Sat Flow, veh/h	5	1702	130	1774	1488	318	157	717	794	862	589	69
Grp Volume(v), veh/h	312	0	0	49	0	210	63	0	0	66	0	.0
Grp Sat Flow(s),veh/h/ln	1837	0	0	1774	0	1807	1668	0	0	1520	0	C
Q Serve (q. s), s	0.0	0.0	0.0	1.1	0.0	3.3	0.0	0.0	0.0	0.0	0.0	0.0
Cycle Q Clear(q_c), s	6.3	0.0	0.0	1.1	0.0	3.3	0.9	0.0	0.0	0.9	0.0	0.0
Prop In Lane	0.01		0.07	1.00		0.18	0.17		0.48	0.62		0.05
Lane Grp Cap(c), veh/h	546	0	0	74	0	701	797	0	0	775	0	0
V/C Ratio(X)	0.57	0.00	0.00	0.66	0.00	0.30	0.08	0.00	0.00	0.09	0.00	0.00
Avail Cap(c a), veh/h	807	0	0	217	0	1105	797	0	0	775	0	0
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Upstream Filter(I)	1.00	0.00	0.00	1.00	0.00	1.00	1.00	0.00	0.00	1.00	0.00	0.00
Uniform Delay (d), s/veh	13.9	0.0	0.0	19.3	0.0	8.7	7.2	0.0	0.0	7.2	0.0	0.0
Incr Delay (d2), s/veh	0.9	0.0	0.0	9.6	0.0	0.2	0.2	0.0	0.0	0.2	0.0	0.0
Initial Q Delay(d3),s/veh	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
%ile Back of Q (50%), veh/ln	2.6	0.0	0.0	0.6	0.0	1.2	0.3	0.0	0.0	0.4	0.0	0.0
Lane Grp Delay (d), s/veh	14.8	0.0	0.0	28.9	0.0	8.9	7.4	0.0	0.0	7.4	0.0	0.0
Lane Grp LOS	В	717		C	V.V.	A	A	- C.	7:7	A	- 3,130	7.7
Approach Vol., veh/h		312			259	-3,50	- 10	63		1000	66	
Approach Delay, s/veh		14.8			12.7			7.4			7.4	
Approach LOS		В			В			А			Α	
Timer		-			-						****	-
Assigned Phs		4		3	8			2			6	
Phs Duration (G+Y+Rc), s		14.2		5.7	19.9			21.0			21.0	
Change Period (Y+Rc), s		4.0		4.0	4.0			4.0			4.0	
Max Green Setting (Gmax), s		16.0		5.0	25.0			17.0			17.0	
Max Q Clear Time (q c+l1), s		8.3		3.1	5.3			2.9			2.9	
Green Ext Time (p_c), s		1.9		0.0	3.1			0.5			0.5	
Intersection Summary												
HCM 2010 Ctrl Delay			12.7									
HCM 2010 LOS			В									
Notes												

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#### 5.2.2 Roundabout control

#### 5.2.2.1 Morning peak hour

#### **MOVEMENT SUMMARY**

Site: Winner at Northern, proposed

Winner at Northern Roundabout

Mov ID											
0 11 1	. II - 51	veh/h	%	v/c	sec		veh	ft		perveh	mpt
	lorthern Bl		42.5	8/2/82	8.8	2022	1200	2023	12.12.23	12022	12.00
3	<u> </u>	5	2.0	0.032	4.0	LOSA	0.1	2.7	0.25	0.79	23.
8	T	11	2.0	0.032	4.0	LOSA	0.1	2.7	0.25	0.28	26.0
18	R	14	2.0	0.032	4.0	LOSA	0.1	2.7	0.25	0.42	25.5
Approac	h	30	2.0	0.032	4.0	LOSA	0.1	2.7	0.25	0.44	25.3
East: Wi	inner Road										
1	L	21	2.0	0.136	4.5	LOSA	0.5	13.1	0.08	0.67	17.8
6	Т	100	2.0	0.136	4.5	LOSA	0.5	13.1	0.08	0.02	18.6
16	R	27	2.0	0.136	4.5	LOSA	0.5	13.1	0.08	0.04	18.5
Approac	h	148	2.0	0.136	4.5	LOSA	0.5	13.1	0.08	0.12	18.4
North: N	lorthern Bh	/d.									
7	L	22	2.0	0.036	4.0	LOSA	0.1	3.1	0.24	0.73	24.2
4	T	12	2.0	0.036	4.0	LOSA	0.1	3.1	0.24	0.34	26.6
14	R	1	2.0	0.036	4.0	LOSA	0.1	3.1	0.24	0.45	26.0
Approac	h	35	2.0	0.036	4.0	LOSA	0.1	3.1	0.24	0.59	25.0
West: W	/inner Roa	i									
5	L	1	2.0	0.117	4.5	LOSA	0.4	11.0	0.16	0.94	25.7
2	T	114	2.0	0.117	4.5	LOSA	0.4	11.0	0.16	0.36	28.7
12	R	8	2.0	0.117	4.5	LOSA	0.4	11.0	0.16	0.51	28.0
Approac	:h	123	2.0	0.117	4.5	LOSA	0.4	11.0	0.16	0.38	28.6
All Vehic	des	336	2.0	0.136	4.4	LOSA	0.5	13.1	0.14	0.29	22.8

Level of Service (LOS) Method: Delay & v/c (HCM 2010).

Roundabout LOS Method: Same as Sign Control.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement LOS F will result if v/c > 1 irrespective of movement delay value (does

Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: US HCM 2010.

HCM Delay Model used. Geometric Delay not included.

Processed: Sunday, August 25, 2013 4:08 31 PM Copyright © 2000-2011 Akcelik and Associates Pty Ltd SIDRA INTERSECTION 5 1.13 2093 www.sidrasolutions.com Project: CilvaersIR3C/Desktopl/Winner at Northern proposed AM.sip 8000824, R 3C DESIGN GROUP, SINGLE

SIDRA ---



#### 5.2.2.2 Afternoon peak hour

#### LANE SUMMARY

Site: Winner at Northern, proposed

Winner at Northern Roundabout

		V2000	of Electrical				D	1 2 2 2	A. Landau and	1 2 2 2 1 2 4	0.50/ David	- ( ( )	1 2 2 2	OI.	A-1-	Davids
							Deg. Satn	Lane Util.	Average Delay	Level of Service	95% Back Vehicles	Distance		SL Type	Cap. Adi.	
South: Nort	hern Blv	d.														
Lane 1	11	22	30	63	2.0	790	0.080	100	5.4	LOSA	0.3	6.9	1600	12	0.0	0.0
Approach	11	22	30	63	2.0		0.080		5.4	LOSA	0.3	6.9				
East: Winne	erRoad															
Lane 1	49	173	37	259	2.0	1068	0.242	100	5.7	LOSA	1.0	26.3	1600	-	0.0	0.0
Approach	49	173	37	259	2.0		0.242		5.7	LOSA	1.0	26.3				
North: North	nern Blv	i.														
Lane 1	41	22	3	66	2.0	875	0.076	100	4.8	LOSA	0.3	6.7	1600	155	0.0	0.0
Approach	41	22	3	66	2.0		0.076		4.8	LOSA	0.3	6.7				
West: Winn	er Road															
Lane 1	3	287	22	312	2.0	988	0.316	100	6.9	LOSA	1.4	36.3	1600	12	0.0	0.0
Approach	3	287	22	312	2.0		0.316		6.9	LOSA	1.4	36.3				
Intersection				700	2.0		0.316		6.1	LOSA	1.4	36.3				

Level of Service (LOS) Method: Delay & v/c (HCM 2010).

Roundabout LOS Method: Same as Sign Control.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010). Roundabout Capacity Model: US HCM 2010. HCM Delay Model used. Geometric Delay not included.

Processed: Saturday, August 24, 2013 7.06.31 AM Copyright © 2000-2011 Alcelik and Associates Pty Ltd SIDRA INTERSECTION 5.1.13.2093 www.sidrasolutions.com Project C:UsersiR3C/Desktopl/Winner at Northern proposed PM.sip 8000824, R 3C DESIGN GROUP, SINGLE





8/25/2013

## 5.3 18th Street removed and 20 year traffic projections

### 5.3.1 Signal control

### 5.3.1.1 Morning peak hour

HCM 2010 Signalized Intersection Summary

	•	-	7	1	-	•	1	<b>†</b>	1	1	Į.	1
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBF
Lane Configurations		43-		7	<b>^</b>			43	12-13-14-14		4	
Volume (veh/h)	1	105	7	19	92	25	5	10	13	20	11	j
Number	7	4	14	3	8	18	5	2	12	1	6	11
Initial Q (Qb), veh	0	0	0	0	0	0	0	0	0	0	0	- 1
Ped-Bike Adj(A_pbT)	1.00		1.00	1.00		1.00	1.00		1.00	1.00		1.0
Parking Bus Adj	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.0
Adj Sat Flow veh/h/ln	190.0	186.3	190.0	186.3	186.3	190.0	190.0	186.3	190.0	190.0	186.3	190.
Lanes	0	1	0	1	1	0	0	- 1	0	0	1	
Cap, veh/h	99	278	18	52	421	115	195	351	378	605	297	
Arrive On Green	0.16	0.16	0.16	0.03	0.30	0.30	0.49	0.49	0.49	0.49	0.49	0.0
Sat Flow, veh/h	8	1721	110	1774	1409	385	166	723	779	916	613	
Grp Volume(v), veh/h	184	0	0	31	0	191	45	0	0	51	0	
Grp Sat Flow(s), veh/h/ln	1839	o o	0	1774	0	1795	1669	0	0	1529	0	
Q Serve(q_s), s	0.0	0.0	0.0	0.6	0.0	3.1	0.0	0.0	0.0	0.0	0.0	0.0
Cycle Q Clear(q_c), s	3.4	0.0	0.0	0.6	0.0	3.1	0.5	0.0	0.0	0.5	0.0	0.0
Prop In Lane	0.01	0.0	0.06	1.00	V.0	0.21	0.18	V.V.	0.47	0.65	Y.Y.	0.0
Lane Grp Cap(c), veh/h	395	0	0.00	52	0	536	924	0	0	902	0	V.V
V/C Ratio(X)	0.47	0.00	0.00	0.59	0.00	0.36	0.05	0.00	0.00	0.06	0.00	0.0
Avail Cap(c a), veh/h	890	0	0.00	191	0	1162	924	0.00	0	902	0.00	V.V.
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.0
Upstream Filter(I)	1.00	0.00	0.00	1.00	0.00	1.00	1.00	0.00	0.00	1.00	0.00	0.0
Uniform Delay (d), s/veh	14.5	0.0	0.0	17.8	0.0	10.2	5.0	0.0	0.0	5.0	0.0	0.0
Incr Delay (d2), s/veh	0.9	0.0	0.0	10.2	0.0	0.4	0.1	0.0	0.0	0.1	0.0	0.0
Initial Q Delay(d3),s/veh	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
%ile Back of Q (50%), veh/ln	1.5	0.0	0.0	0.4	0.0	1.2	0.0	0.0	0.0	0.2	0.0	0.0
Lane Grp Delay (d), s/veh	15.3	0.0	0.0	28.0	0.0	10.6	5.1	0.0	0.0	5.2	0.0	0.0
Lane Grp LOS	В	۷.۷	0.0	C	V.V	В	A	0.0	V.V	Α.	٧.٧	V.5
Approach Vol., veh <i>i</i> h		184		- 3	222	ь		45		-0	51	
Approach Vol, verm Approach Delay, s/veh		15.3			13.0			5.1			5.2	
Approach LOS		10.5 B			13.0 B			Α.			3.2 A	
		, ,			U						0	
Timer												
Assigned Phs		4		3	8			2			6	
Phs Duration (G+Y+Rc), s		10.0		5.1	15.1			22.0			22.0	
Change Period (Y+Rc), s		4.0		4.0	4.0			4.0			4.0	
Max Green Setting (Gmax), s		16.0		4.0	24.0			18.0			18.0	
Max Q Clear Time (g_c+l1), s		5.4		2.6	5.1			2.5			2.5	
Green Ext.Time (p_c),s		0.7		0.1	1.1			0.4			0.4	
Intersection Summary												
HCM 2010 Ctrl Delay			12.4									
HCM 2010 LOS			В									

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### 5.3.1.2 Afternoon peak hour

HCM 2010 Signalized Intersection Summary

8			

	1	-	7	1	$\leftarrow$	*	1	<b>†</b>	1	1	ļ	1
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBF
Lane Configurations		4		7	1			43	12-12-20-20-20-20-20-20-20-20-20-20-20-20-20	- Contract	4	
Volume (veh/h)	3	264	20	45	159	34	10	20	28	38	20	3
Number	7	4	14	3	8	18	5	2	12	1	6	16
Initial Q (Qb), veh	0	0	0	0	0	0	0	0	0	0	0	0
Ped-Bike Adj(A_pbT)	1.00		1.00	1.00		1.00	1.00		1.00	1.00		1.00
Parking Bus Adj	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Adj Sat Flow veh/h/In	190.0	186.3	190.0	186.3	186.3	190.0	190.0	186.3	190.0	190.0	186.3	190.0
Lanes	0	1	0	1	1	0	0	1	0	0	1	0
Cap, veh/h	81	540	41	94	681	145	146	263	298	441	214	28
Arrive On Green	0.32	0.32	0.32	0.05	0.46	0.46	0.37	0.37	0.37	0.37	0.37	0.37
Sat Flow, weh/h	5	1701	129	1774	1490	316	148	712	807	852	580	75
Grp Volume(v), veh/h	468	0	0	73	0	314	95	0	0	100	0	0
Grp Sat Flow(s), veh/h/ln	1836	0	0	1774	0	1807	1666	0	0	1508	0	0
Q Serve (q. s), s	0.2	0.0	0.0	1.9	0.0	5.3	0.0	0.0	0.0	0.0	0.0	0.0
Cycle Q Clear(q_c), s	10.7	0.0	0.0	1.9	0.0	5.3	1.7	0.0	0.0	1.7	0.0	0.0
Prop In Lane	0.01		0.07	1.00		0.18	0.17		0.48	0.62		0.05
Lane Grp Cap(c), veh/h	662	0	0	94	0	826	706	0	0	683	0	0
V/C Ratio(X)	0.71	0.00	0.00	0.78	0.00	0.38	0.13	0.00	0.00	0.15	0.00	0.00
Avail Cap(c a), veh/h	756	0	0	154	0	981	706	0	0	683	0	0
HCM Platoon Ratio	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Upstream Filter(I)	1.00	0.00	0.00	1.00	0.00	1.00	1.00	0.00	0.00	1.00	0.00	0.00
Uniform Delay (d), s/veh	14.4	0.0	0.0	21.6	0.0	8.2	9.7	0.0	0.0	9.7	0.0	0.0
Incr Delay (d2), s/veh	2.6	0.0	0.0	13.1	0.0	0.3	0.4	0.0	0.0	0.5	0.0	0.0
Initial Q Delay(d3),s/veh	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
%ile Back of Q (50%), veh/ln	4.8	0.0	0.0	1.1	0.0	1.9	0.7	0.0	0.0	0.8	0.0	0.0
Lane Grp Delay (d), s/veh	17.0	0.0	0.0	34.6	0.0	8.5	10.1	0.0	0.0	10.1	0.0	0.0
Lane Grp LOS	В			С		Α	В			В		
Approach Vol, veh/h		468		0.00	387	20700		95			100	
Approach Delay, s/veh		17.0			13.4			10.1			10.1	
Approach LOS		В			В			В			В	
Timer												
Assigned Phs		4		3	8			2			6	
Phs Duration (G+Y+Rc), s		18.6		6.4	25.1			21.0			21.0	
Change Period (Y+Rc), s		4.0		4.0	4.0			4.0			4.0	
Max Green Setting (Gmax), s		17.0		4.0	25.0			17.0			17.0	
Max Q Clear Time (q c+l1), s		12.7		3.9	7.3			3.7			3.7	
Green Ext Time (p_c), s		1.9		0.0	4.8			0.8			0.8	
Intersection Summary												
HCM 2010 Ctrl Delay			14.4									
HCM 2010 LOS			В									
Notes												

Baseline Synchro \$ Report
Page 1



#### 5.3.2 Roundabout control

#### 5.3.2.1 Morning peak hour

#### **MOVEMENT SUMMARY**

Site: Winner at Northern, future AM

Winner at Northern Roundabout

Design Life Analysis (Practical Capacity): Results for 20 years

											Average
Mov ID					Delay			Distance			
	NAMES AND ADDRESS OF THE PARTY	veh/h	%	v/c	sec		veh	ft		perveh	mpt
South: N	lorthern B										
3	L	8	2.0	0.047	4.4	LOSA	0.2	4.0	0.30	0.79	23.5
8	T	15	2.0	0.047	4.4	LOSA	0.2	4.0	0.30	0.33	25.8
18	R	20	2.0	0.047	4.4	LOSA	0.2	4.0	0.30	0.45	25.3
Approac	h	43	2.0	0.047	4.4	LOSA	0.2	4.0	0.30	0.47	25.1
East: Wi	nner Roa	d									
1	L	29	2.0	0.192	5.1	LOSA	0.8	19.6	0.11	0.66	17.6
6	T	140	2.0	0.192	5.1	LOSA	0.8	19.6	0.11	0.03	18.4
16	R	38	2.0	0.192	5.1	LOSA	0.8	19.6	0.11	0.05	18.3
Approac	h	207	2.0	0.192	5.1	LOSA	0.8	19.6	0.11	0.12	18.3
North: N	orthern B	lvd.									
7	L	30	2.0	0.053	4.4	LOSA	0.2	4.6	0.29	0.74	24.1
4	T	17	2.0	0.053	4.4	LOSA	0.2	4.6	0.29	0.38	26.4
14	R	2	2.0	0.053	4.4	LOSA	0.2	4.6	0.29	0.48	25.8
Approac	h	49	2.0	0.053	4.4	LOSA	0.2	4.6	0.29	0.61	24.8
West: W	inner Roa	ad									
5	L	2	2.0	0.168	5.1	LOSA	0.7	16.5	0.20	0.92	25.5
2	T	160	2.0	0.168	5.1	LOSA	0.7	16.5	0.20	0.38	28.4
12	R	11	2.0	0.168	5.1	LOSA	0.7	16.5	0.20	0.52	27.7
Approac	h	172	2.0	0.168	5.1	LOSA	0.7	16.5	0.20	0.40	28.3
All Vehic	des	470	2.0	0.192	4.9	LOSA	0.8	19.6	0.18	0.30	22.6

Level of Service (LOS) Method: Delay & v/c (HCM 2010).

Roundabout LOS Method: Same as Sign Control.

Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement

LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection). Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: US HCM 2010.

HCM Delay Model used. Geometric Delay not included.

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#### 5.3.2.2 Afternoon peak hour

#### **LANE SUMMARY**

Site: Winner at Northern, future PM

Winner at Northern Roundabout

Design Life Analysis (Practical Capacity): Results for 20 years

Lane Use																
		Demar T	id Flows R				Deg. Satn	Lane Util.	Average Delay		95% Back Vehicles	of Queue Distance	Lane Length			
		veh/h	veh/h	veh/h	%	veh/h	v/c	%	sec		veh	ft	ft	62 HZ	%	%
South: Nort	hern Bl	rd.														
Lane 1	15	30	43	88	2.0	690	0.128	100	6.6	LOSA	0.4	11.2	1600	-	0.0	0.0
Approach	15	30	43	88	2.0		0.128		6.6	LOSA	0.4	11.2				
East: Winne	erRoad															
Lane 1	68	242	52	362	2.0	1053	0.344	100	6.9	LOSA	1.7	42.4	1600	-	0.0	0.0
Approach	68	242	52	362	2.0		0.344		6.9	LOSA	1.7	42.4				
North: North	hern Blv	d.														
Lane 1	58	30	5	93	2.0	795	0.117	100	5.7	LOSA	0.4	10.4	1600	14	0.0	0.0
Approach	58	30	5	93	2.0		0.117		5.7	LOSA	0.4	10.4				
West: Winn	er Road	ľ														
Lane 1	5	402	30	437	2.0	944	0.462	100	9.4	LOSA	2.5	62.6	1600	-	0.0	0.0
Approach	5	402	30	437	2.0		0.462		9.4	LOSA	2.5	62.6				
Intersection	i			980	2.0		0.462		7.9	LOSA	2.5	62.6				

Level of Service (LOS) Method: Delay & v/c (HCM 2010).

Roundabout LOS Method: Same as Sign Control.

Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.

LOS F will result if v/c > irrespective of lane delay value (does not apply for approaches and intersection).

Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).

Roundabout Capacity Model: US HCM 2010.

HCM Delay Model used. Geometric Delay not included.

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